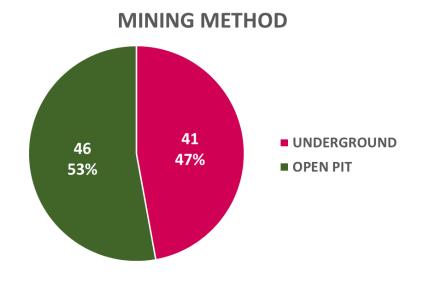


PRESENTATION OUTLINE

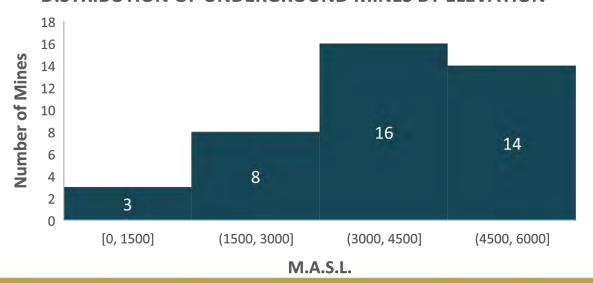
- 1. Mining in Peru and the Andes
- 2. Modern Mine Ventilation System Design
- 3. Prefeasibility Base Model
- 4. Case Study Conditions
- 5. Feasibility Study: Opportunities for Improvement
- 6. Results and LOM Simulation
- 7. Conclusions
- 8. Future Work



Mining in Peru



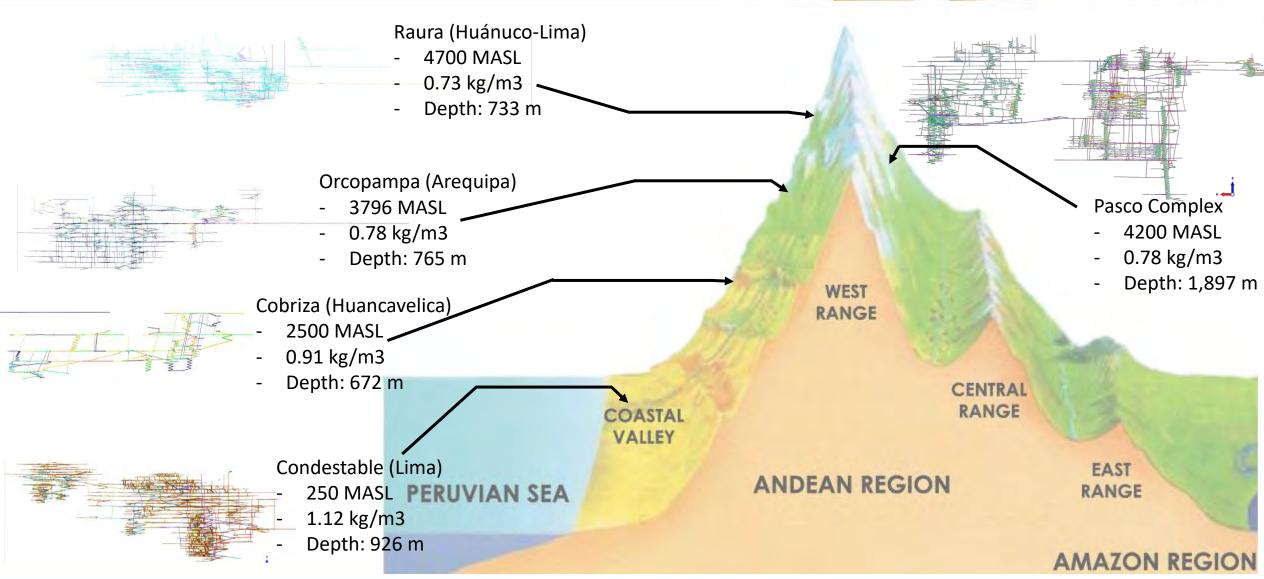
DISTRIBUTION OF UNDERGROUND MINES BY ELEVATION





Mining in the Andes









Modern Mine Ventilation System Design

Sequenced Modelling







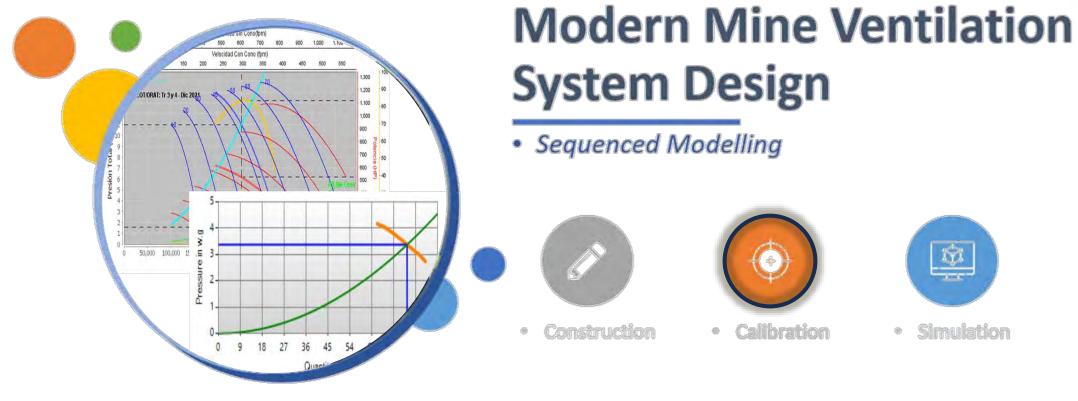


BUILD-UP THE MODEL

- Create the airways based on the mine maps
- Adjust the dimensions for each excavation
- Define the openings and the close ends

Modern Mine Ventilation System Design



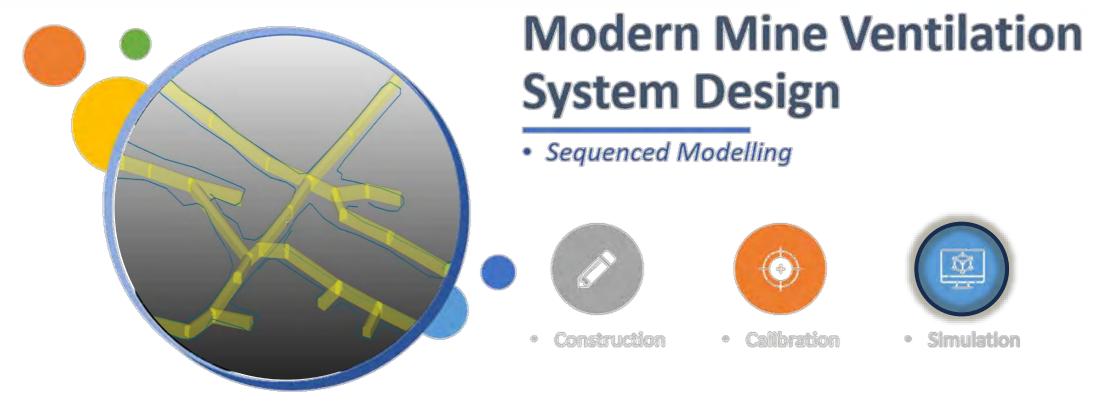


CALIBRATION

- Adjust environmental conditions
- Add & Set up fans to operational parameters
 - Adjust resistances and friction factors

Modern Mine Ventilation System Design



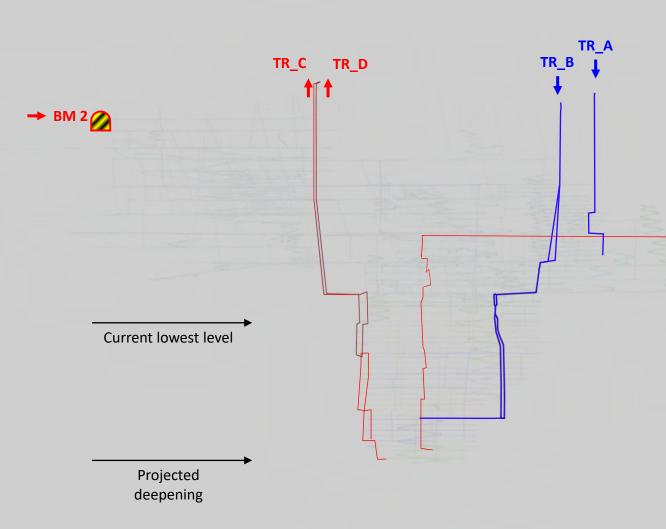


SIMULATION STAGE FOR LONG-TERM PLANNING

- Model able to simulate feasible scenarios
- Ventilation design aligned with production forecast
 - Accurate simulation of power consumption







MINE CONDITIONS:

• Elevation : 4,799 MASL

• Extension : 4,667 m

• Current Depth : 733 m

• Projected Depth : 1,256 m

Mining Method : Sublevel Stoping

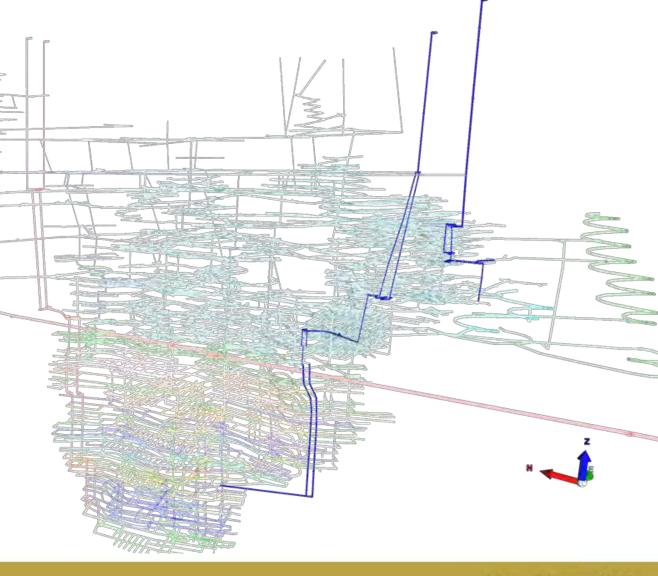
• Hauling Equipment : Trucks



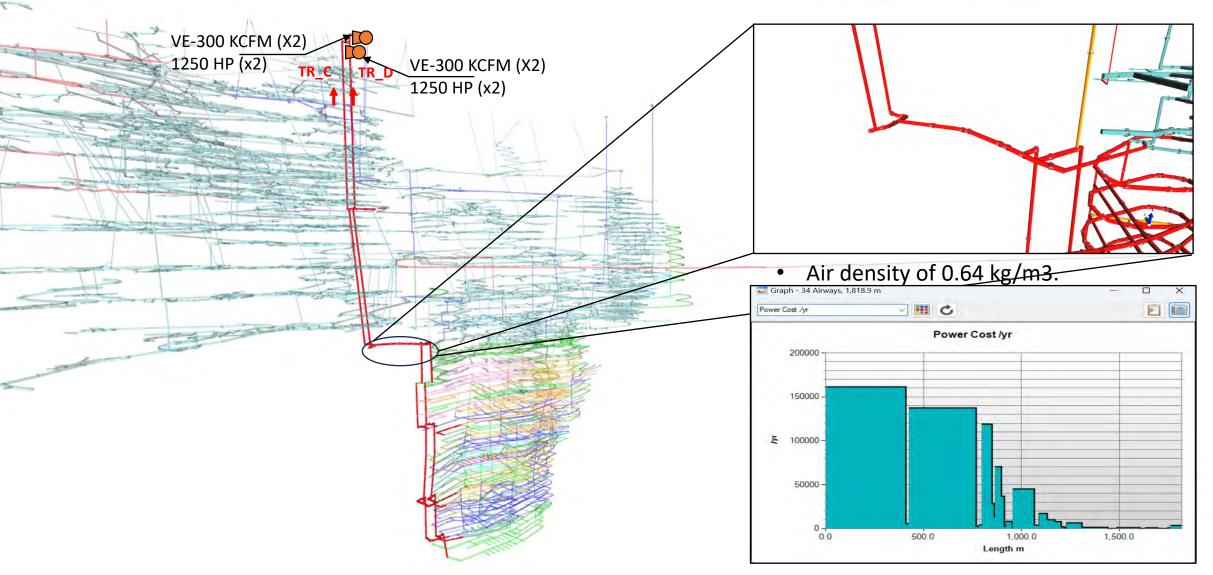


INTAKE CIRCUIT:

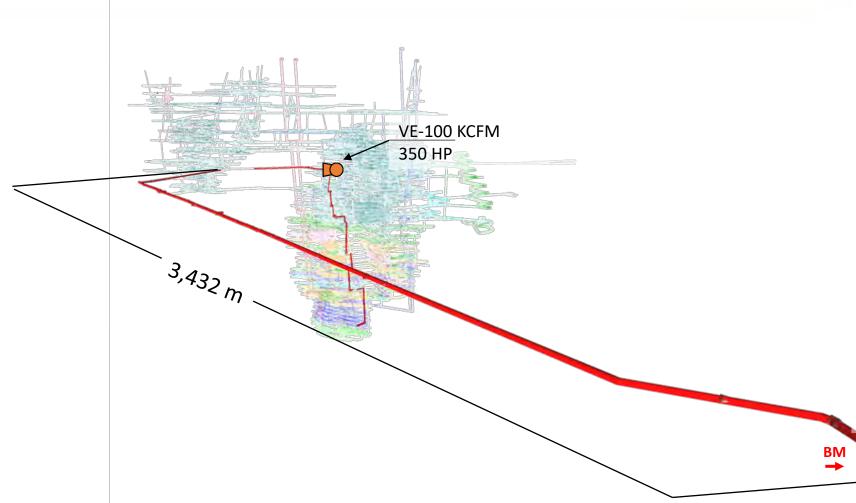
- Zoned (South).
- Vertical distance of 1,340 m
- Two parallel circuits directed to the same zone.
- Defined main levels.
- Effective fresh-air circuit to the bottom level.
- Air density of 0.64 kg/m3.









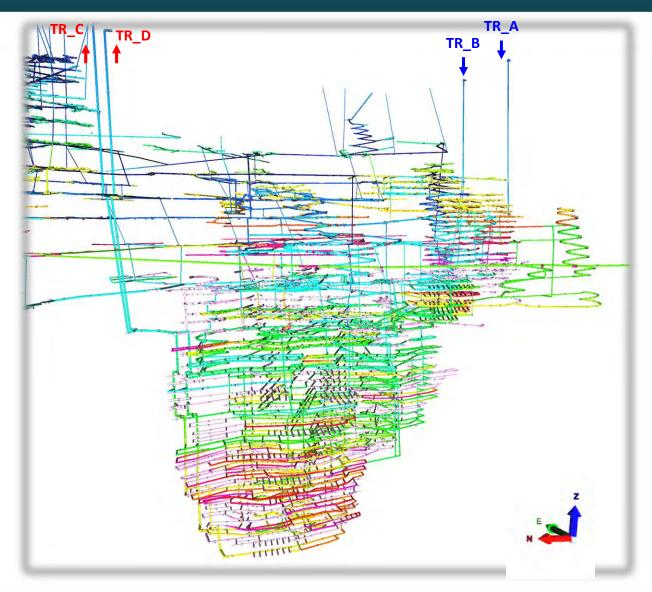


EXHAUST CIRCUIT:

- Zoned (North).
- Horizontal distance of 3,432 m.
- Exhaust through mid-upper zone towards portal (BM).
- Air density of 0.64 kg/m3.

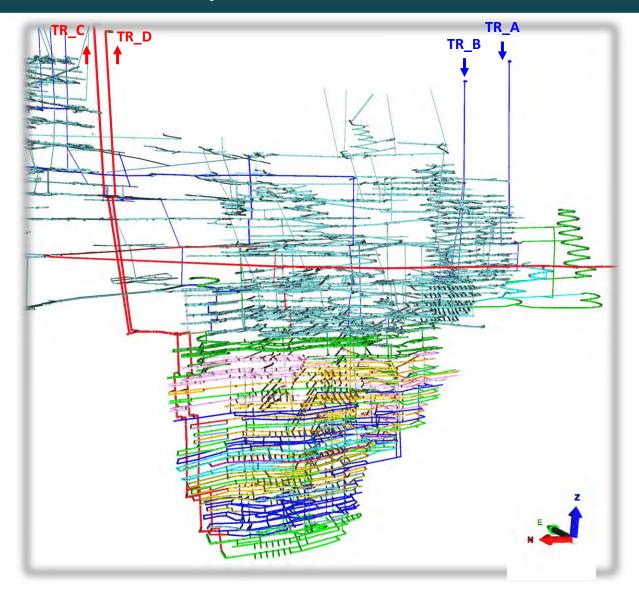






Environment	
Air Density Compressible Flow	0.64 kg/m ³
Air Density Incompressible Flow	0.64 kg/m ³
Surface Temperature Adjust	Si
Current Year	2021.515
Rock Specific Heat	790.0 J/kgC
Rock Thermal Conductivity	2.00 W/mC
Rock Density	2.700 kg/m ³
Rock Thermal Diffusivity	0.938 m ² /s 10-6
Airway Age	5.000 years
Surface Datum of MineGrid	4,866.4 m
Rock Wetness Fraction	0.15
Geothermal Gradient	2.5 C/100m
Surface Datum Pressure Barometric	56.221 kPa
Surface Atmospheric Lapse Rate	6.4 C/1000m
Surface Datum Relative Humidity	39.7 R
Surface Datum Elevation Above Sea Level	4,700.0 m
Surface Datum Rock Temperature	20.0 C
Surface Datum Temperature Wet Bulb	20.0 C
Surface Datum Temperature Dry Bulb	30.0 C

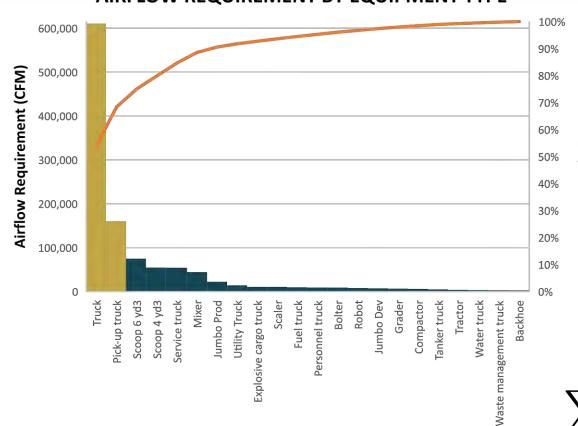


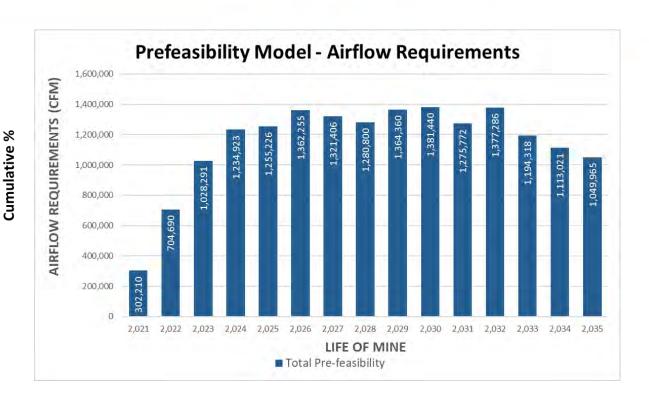


Friction Factors (kg/m³)	
Custom	
Auto	
*Raises	0.013
*Airways	0.01
*Ramps	0.014
*RaiseBored Airway	0.005
Smooth Blasted	0.0085
Average Blasted	0.012
Rough Blasted	0.015
Very Rough Blasted	0.02
Concrete Lined Airway	0.0033
Concrete Shaft Sets	0.0417
Timbered Airway	0.0333
Flexible Duct	0.0029



AIRFLOW REQUIREMENT BY EQUIPMENT TYPE





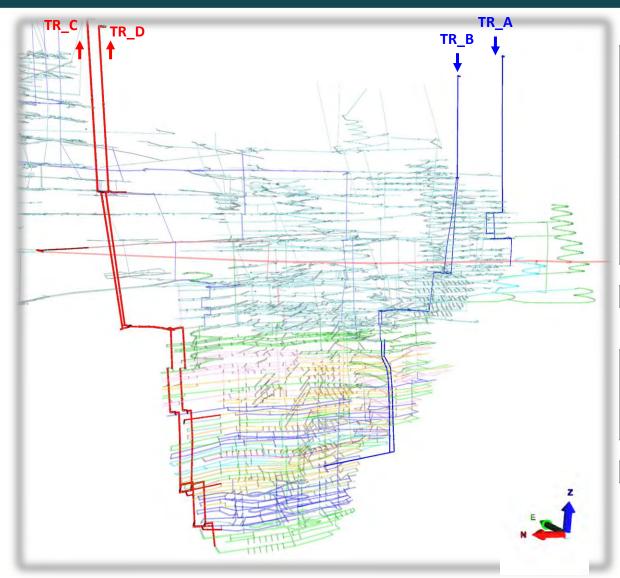
 $\sum \frac{[(Diesel\ Equipment + Workers + Temperature\ Control + \\ Wood\ Consumption) + \textbf{Leaks}\ (\textbf{15}\%)]}{}$

Type of equipment

D.S.N°024-2016 and modifications from D.S.N°023-2017:

§ ART. 252 (d) "The airflow requirements in the mine must be the sum of the airflow required by workers, the airflow to maintain appropriate temperature conditions in the working area and the airflow for the operation of diesel equipment. If there is no diesel equipment in the mine, it must be considered instead the airflow required to ensure gas dilution from the blasting, in accordance with the guidelines from Annex 38".





Prefeasibility Study - CAPEX					
Component / Activity		Escalated value			
Ventilation Infrastructure					
Ventilation Circuit - TRONCAL TR 03	\$	6,097,892			
Ventilation Circuit - TRONCAL TR 04	\$	6,258,108			
Secondary Ventilation System	\$	2,866,347			
Power Distribution System					
Electric Substation + Distribution No. 01 (TR 03 + TR 04)	\$	7,852,259			
Electric Substation + Distribution No. 02 (Secondary System)	\$	225,374			

Prefeasibility Study - OPEX					
Component / Activity	Escalated value				
Power consumption	\$ 22,320,716				
NPV OPE	\$ 11,201,248				

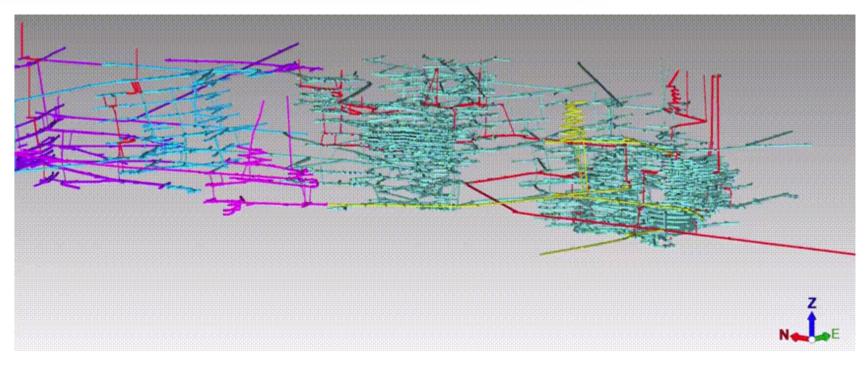
CAPEX PFS

IRR: annual 12 %

\$ 23,299,979

Case Study Conditions







Main Portal Elevation at 4,800 MASL



Air Density: 0.73 kg/m3



Barometric Pressure: ~58,270 Pa



Dry Temperature: 2.36 - 11.20 °C



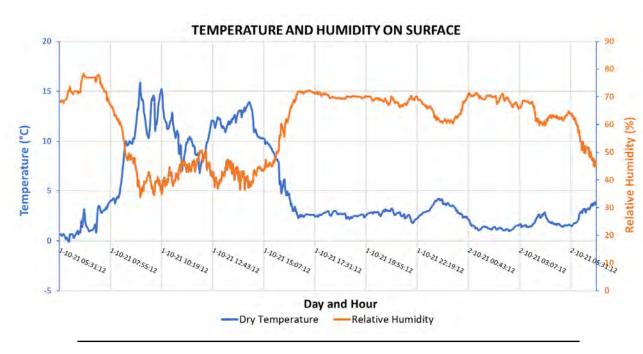
Relative Humidity: 43 - 67 %



Power Cost: 0.072 US\$/Kw-hr

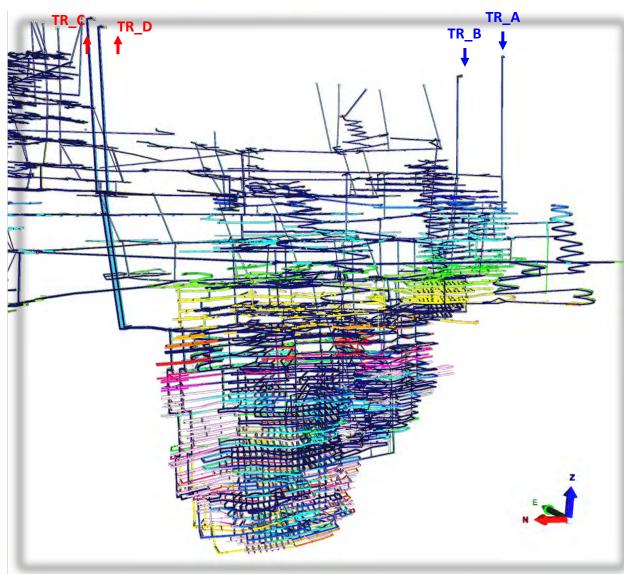






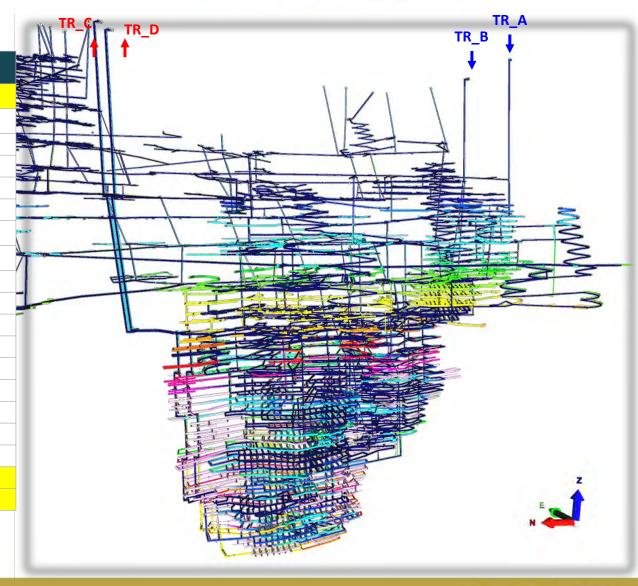
AVERAGE VALUES

	Dry Temperature (°C)	Relative Humidity (%)	Barometric Pressure (Pa)
AVG Day	11.20	42.85	58,282.91
AVG Night	2.60	39.7	58,260.32
Prefeasibility	30.0	39.7	56,221.00





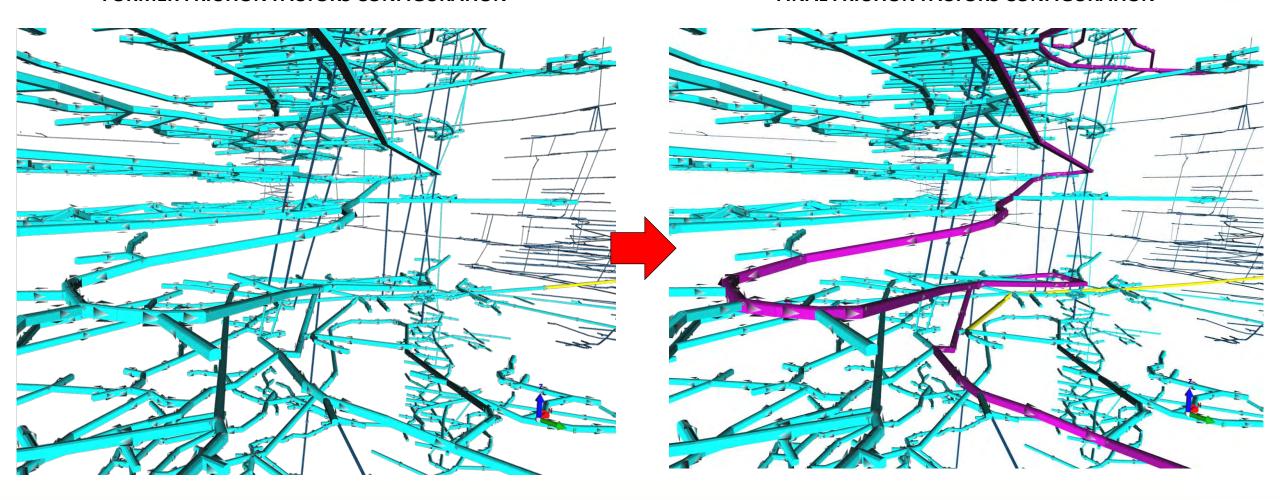
Environment	PFS	FS
Air Density Compressible Flow	0.64 kg/m ³	0.73 kg/m ³
Air Density Incompressible Flow	0.64 kg/m ³	0.64 kg/m ³
Surface Temperature Adjust	Si	Si
Current Year	2021.515	2021.515
Rock Specific Heat	790.0 J/kgC	790.0 J/kgC
Rock Thermal Conductivity	2.00 W/mC	2.00 W/mC
Rock Density	2.700 kg/m ³	2.700 kg/m ³
Rock Thermal Diffusivity	0.938 m ² /s 10-6	0.938 m ² /s 10-6
Airway Age	5.000 years	5.000 years
Surface Datum of MineGrid	4,866.4 m	4,866.4 m
Rock Wetness Fraction	0.15	0.15
Geothermal Gradient	2.5 C/1000m	2.5 C/1000m
Surface Datum Pressure Barometric	56.221 kPa	56.221 kPa
Surface Atmospheric Lapse Rate	6.4 C/1000m	6.4 C/1000m
Surface Datum Relative Humidity	39.7 R	39.7 R
Surface Datum Elevation Above Sea Level	4,700.0 m	4,700.0 m
Surface Datum Rock Temperature	20.0 C	20.0 C
Surface Datum Temperature Wet Bulb	20.0 C	-0.3 C
Surface Datum Temperature Dry Bulb	30.0 C	2.6 C





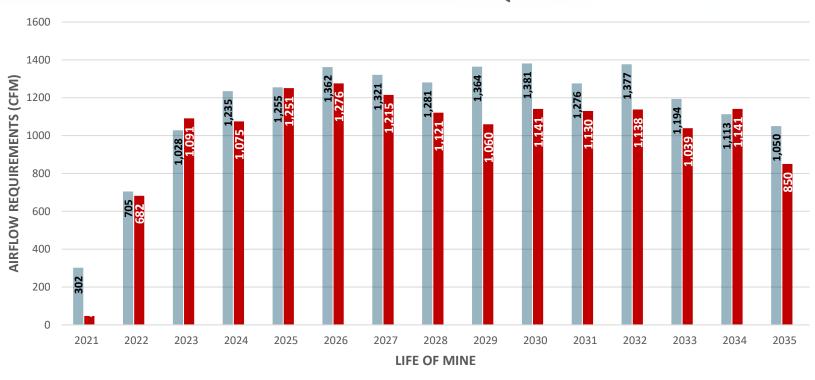
FORMER FRICTION FACTORS CONFIGURATION

FINAL FRICTION FACTORS CONFIGURATION





FEASIBILITY MODEL - AIRFLOW REQUIREMENTS

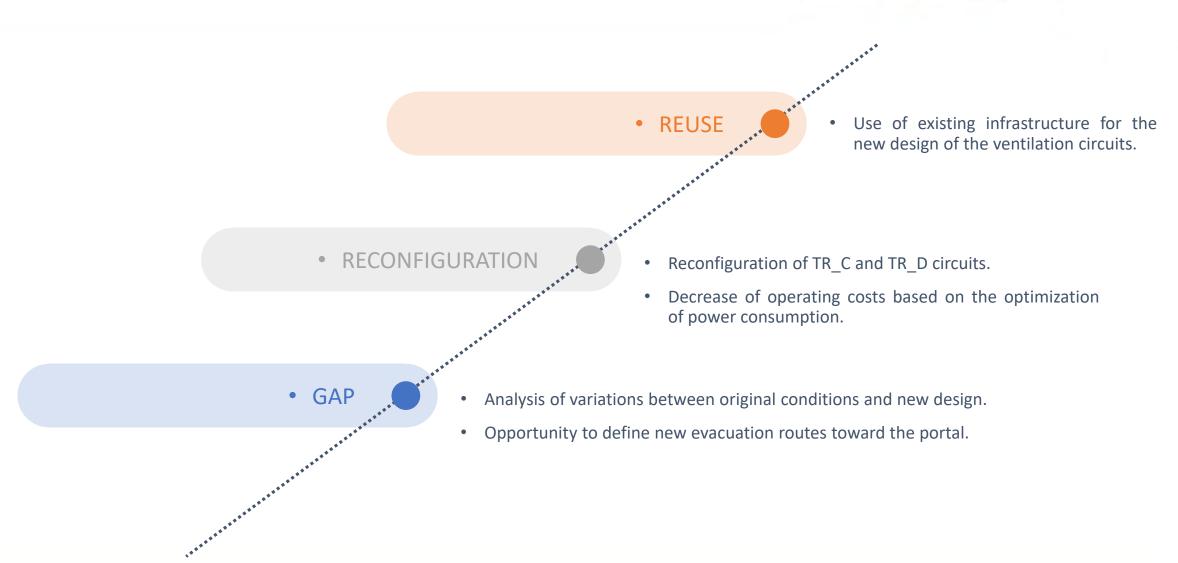


■ Total Pre-Feasibility ■ Total Feasibility

	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035
Total Pre-Feasibility (KCFM)	302	705	1,028	1,235	1,255	1,362	1,321	1,281	1,364	1,381	1,276	1,377	1,194	1,113	1,050
Total Feasibility (KCFM)	47	682	1,091	1,075	1,251	1,276	1,215	1,121	1,060	1,141	1,130	1,138	1,039	1,141	850







VE-250 KCFM (X2)

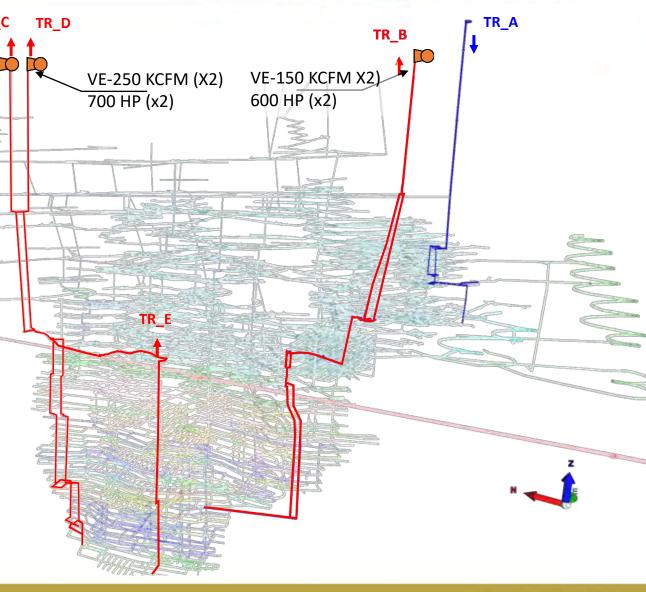
700 HP (x2)



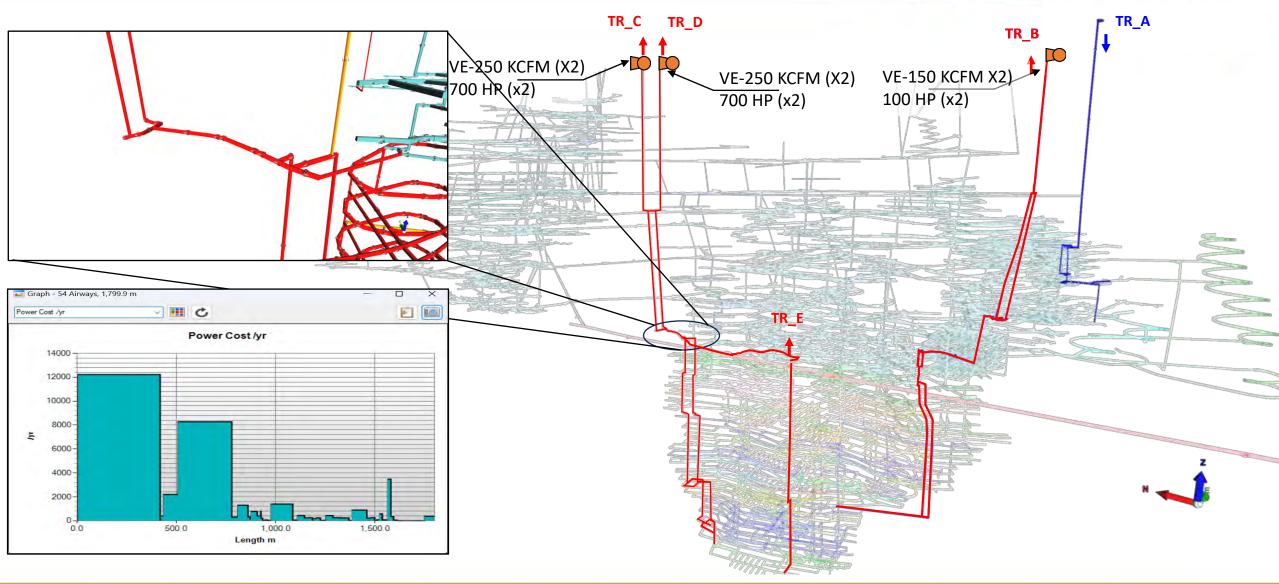
REDISTRIBUTION:

- Zoned (Lower levels).
- Vertical distance of 1,340 m.
- Single intake circuit towards the lower levels.
- Effective fresh-air circuit to the bottom level.
- Air density of 0.73 kg/m3.

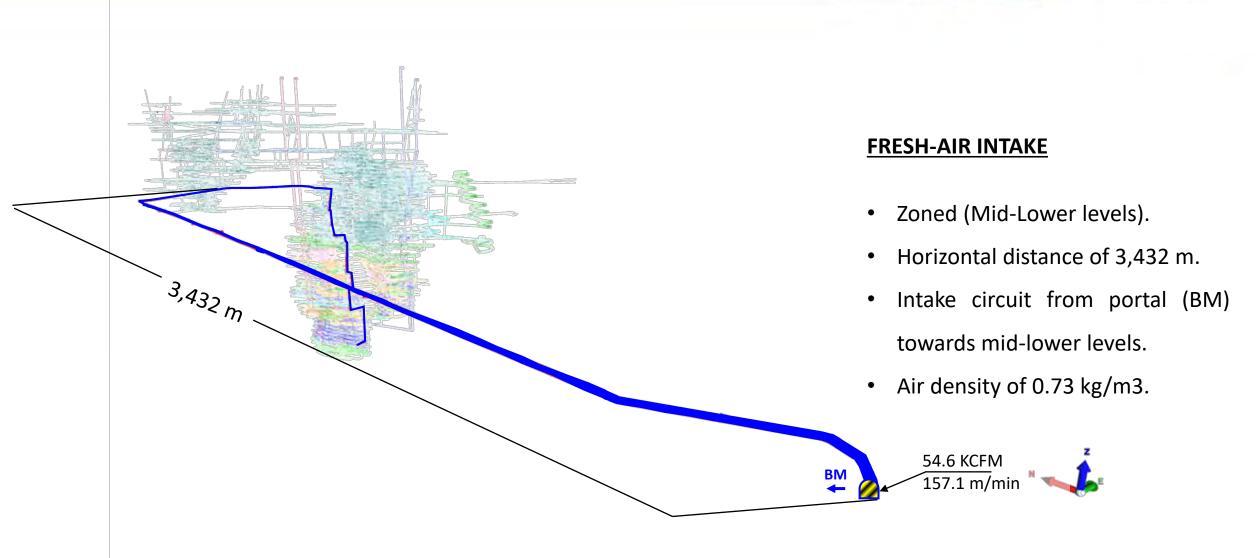
 $P \& Q^{3}$









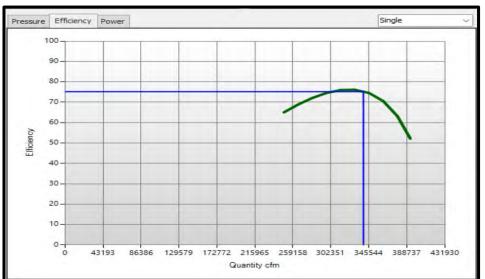


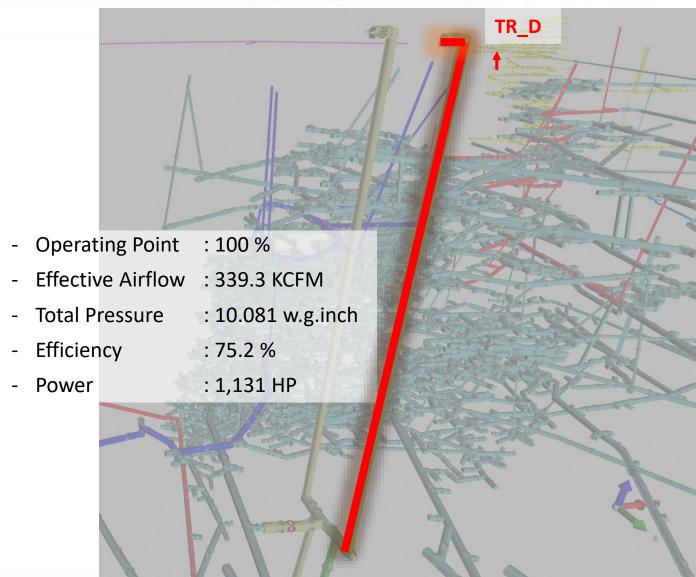


Fan curve – Prefeasibility (2032)



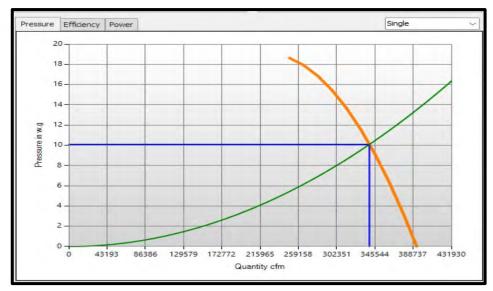


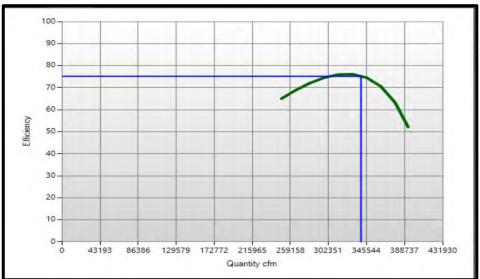


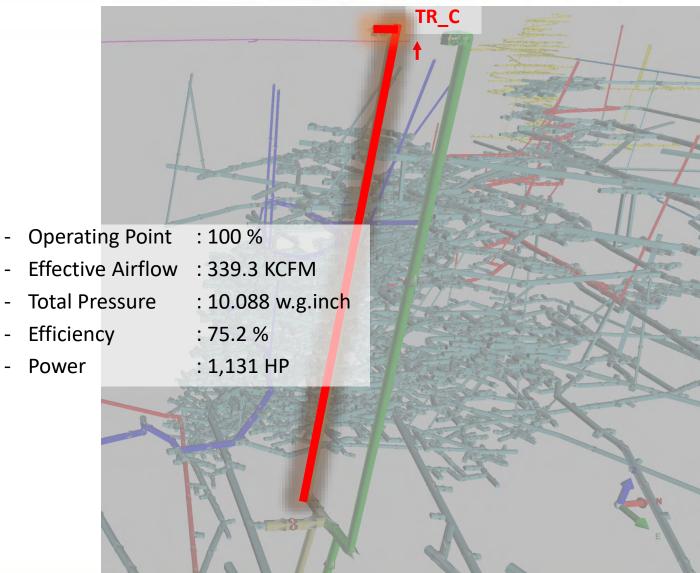


Fan curve – Prefeasibility (2032)



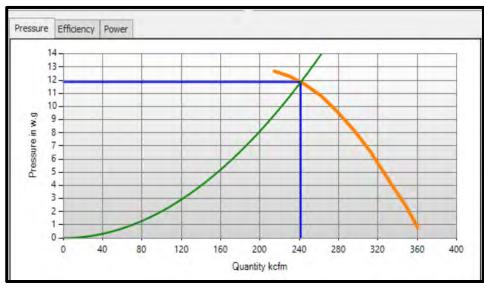


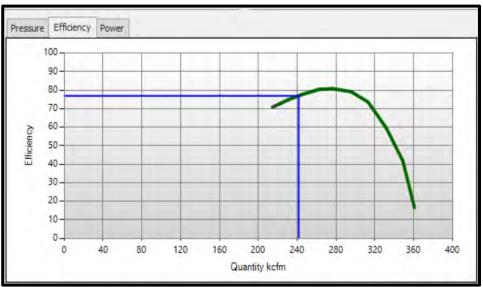


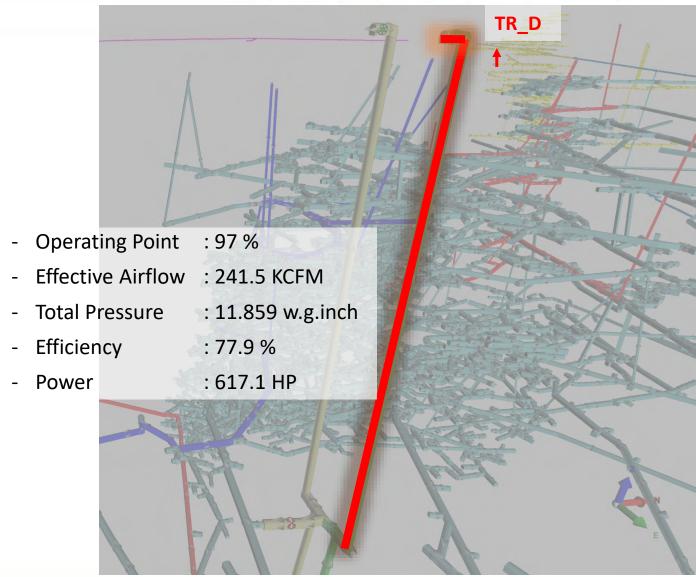


Fan curve – Feasibility (2032)



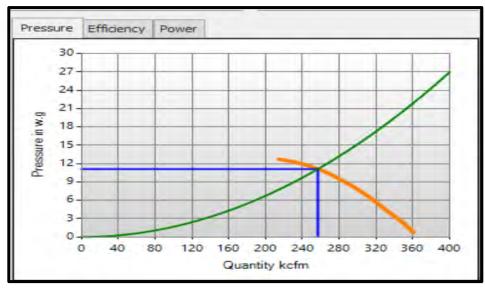


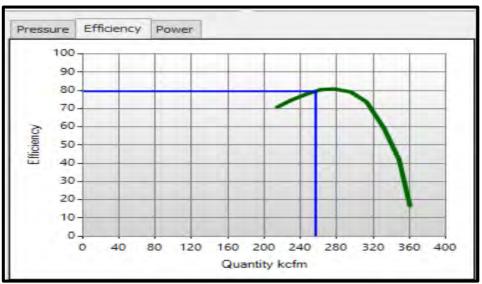


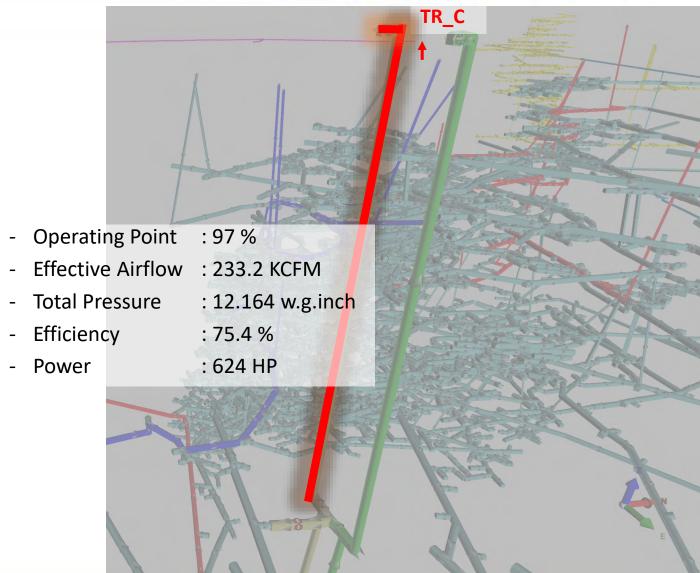


Fan curve – Feasibility (2026)



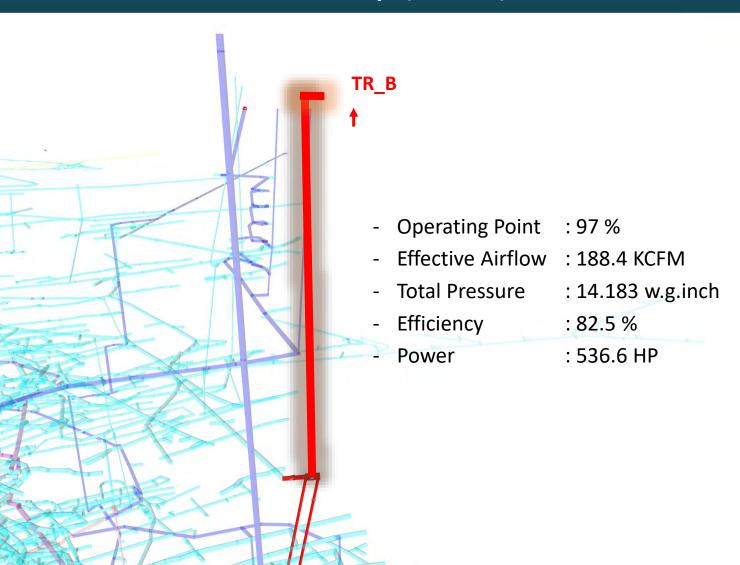


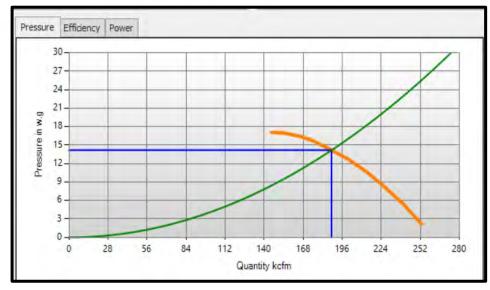


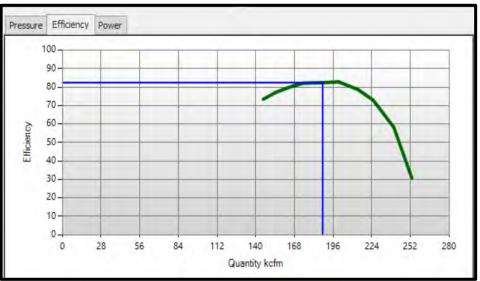


Fan curve – Feasibility (2026)









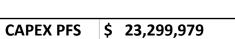
Results



Prefeasibility Study - CAPEX					
Component / Activity		Escalated value			
Ventilation Infrastructure					
Ventilation Circuit - TRONCAL TR 03	\$	6,097,892			
Ventilation Circuit - TRONCAL TR 04	\$	6,258,108			
Secondary ventilation System	\$	2,866,347			
Power Distribution System					
Electric Substation + Distribution No. 01 (TR 03 + TR 04)	\$	7,852,259			
Electric Substation + Distribution No. 02 (Secondary System)	\$	225,374			

reasibility Study - CAPLX						
Component/ Activity	Escaleted Value					
Ventilation Infrastructure						
Ventilation Circuit-TRONCAL TR 02	\$	1,699,152				
Ventilation Circuit-TRONCAL TR 03	\$	1,791,015				
Ventilation Circuit-TRONCAL TR 04	\$	1,783,941				
Power Distribution System						
Electric Substation + Distribution N° 01 (TR 03 + TR 04)	\$	7,852,259				
Ventilation Circuit-TRONCAL TR 04 Power Distribution System	\$	1,783,941				

Feasibility Study - CAPEX



CAPEX FS \$ 13,126,367

Prefeasibility Study - OPEX					
Component / Activity Escalated value					
Power Consumption	\$ 22,320,716				

Feasibility Study - OPEX				
Component / Activity	Escalated value			
Power Consumption	\$ 12,928,244			

NPV OPEX	\$ 11,201,248

NPV OPEX	\$ 6,554,564	

TIR: 12 % annual

CAPEX Savings : \$ 10,173,612
OPEX Savings : \$ 4,646,683
TOTAL Savings : \$ 14,820,295



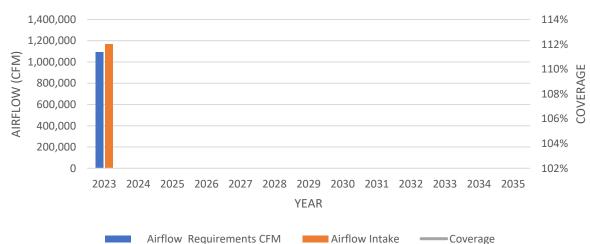
Results – Simulation Stage





YEAR ID

COVERAGE PER YEAR





114%

112%

110% 贳

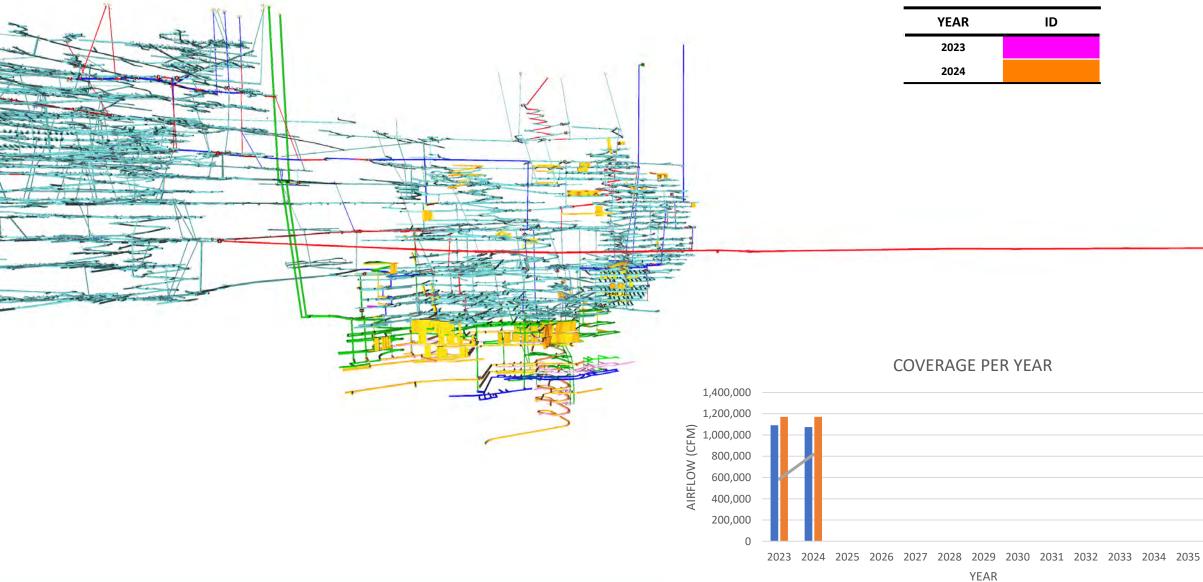
108% H

104%

102%

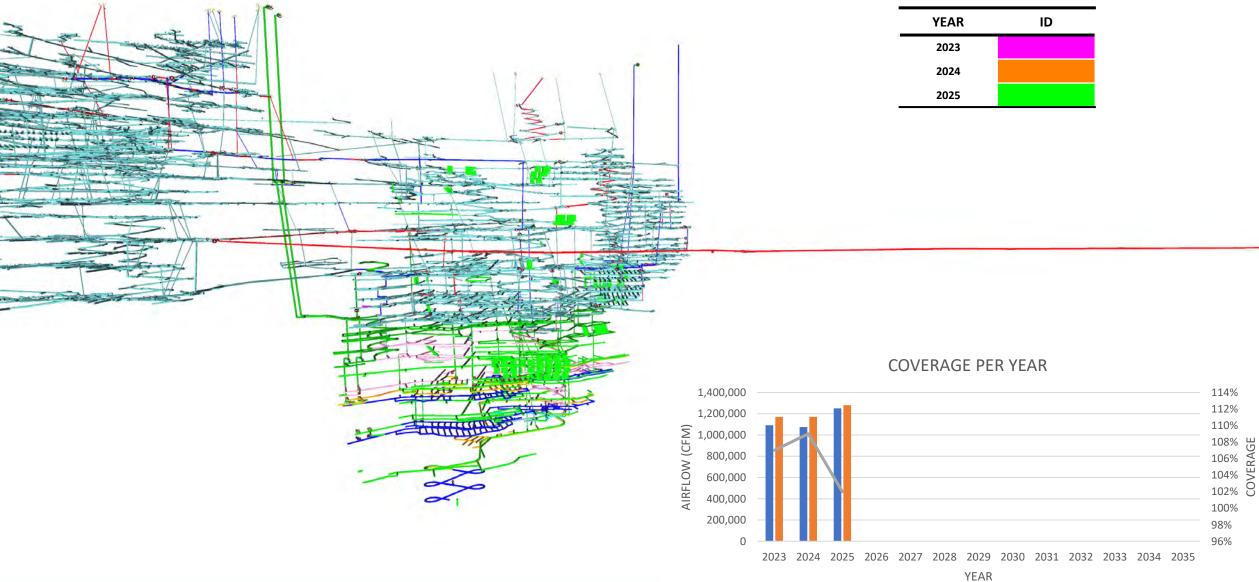
Airflow Requirements CFM

Airflow Intake



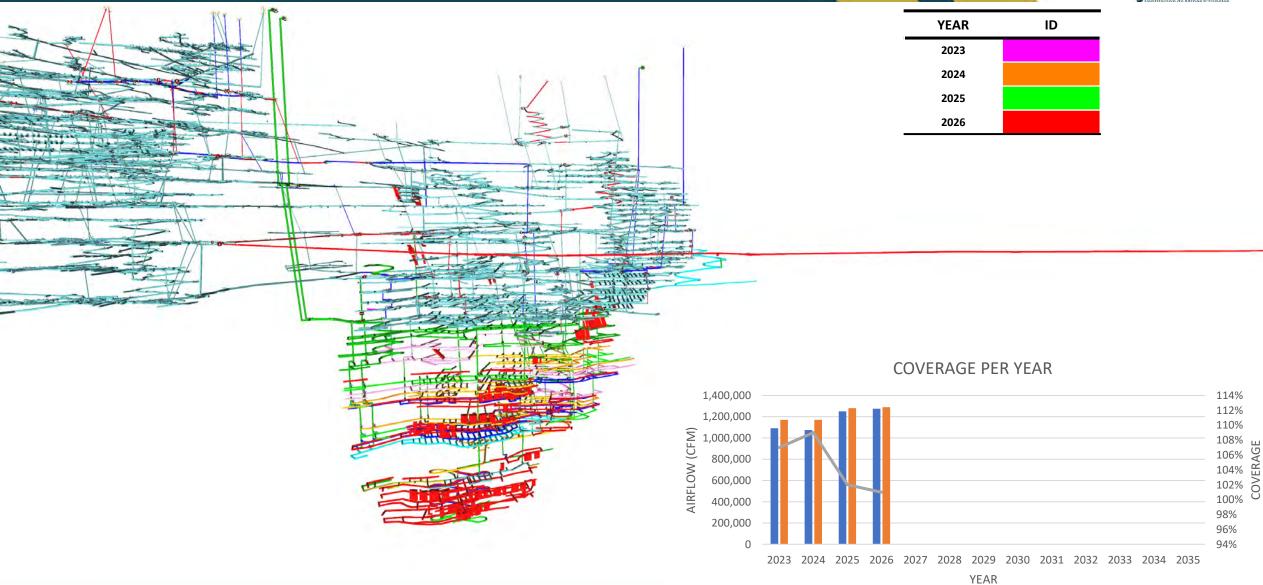


Airflow Requirements CFM Airflow Intake



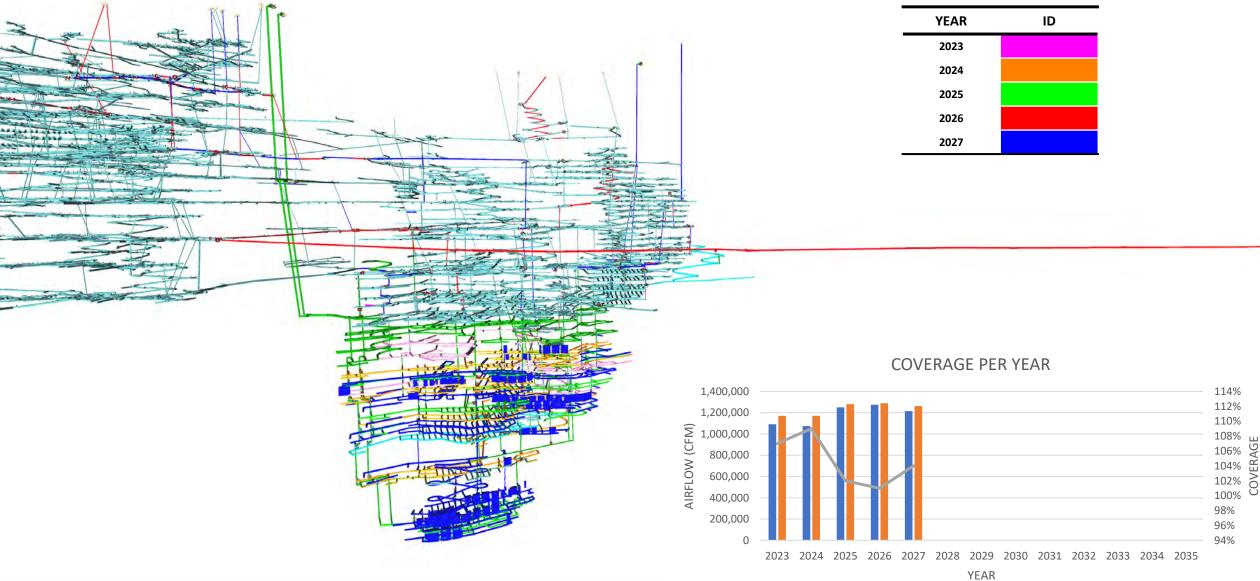


Airflow Requirements CFM Airflow Intake





Airflow Requirements CFM Airflow Intake

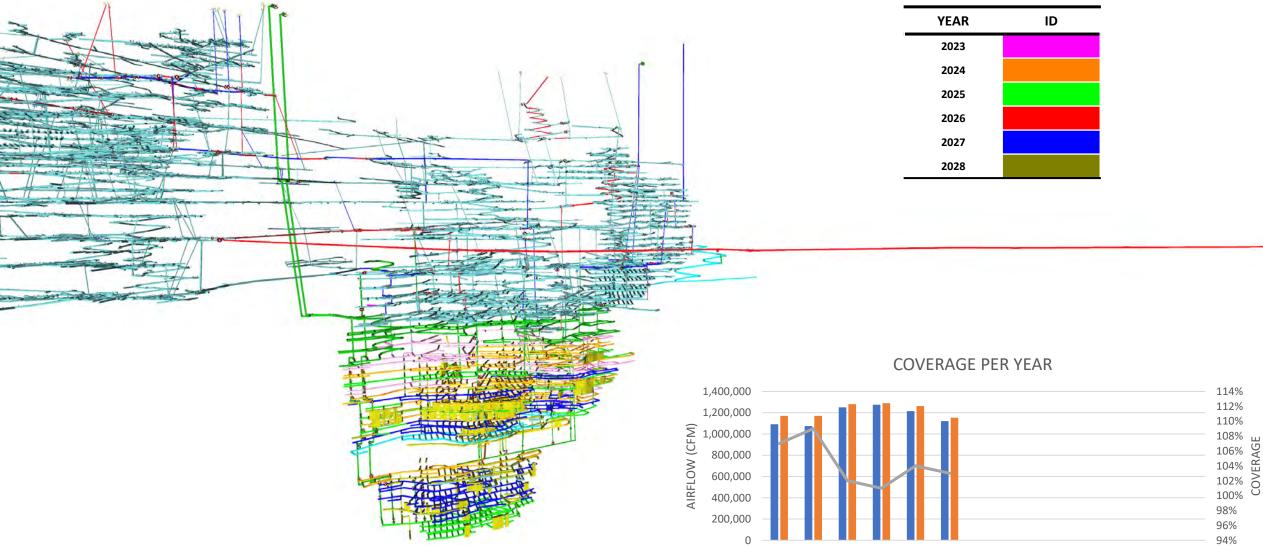




2023 2024 2025 2026 2027 2028 2029 2030 2031 2032 2033 2034 2035 YEAR

Coverage

Airflow Requirements CFM Airflow Intake

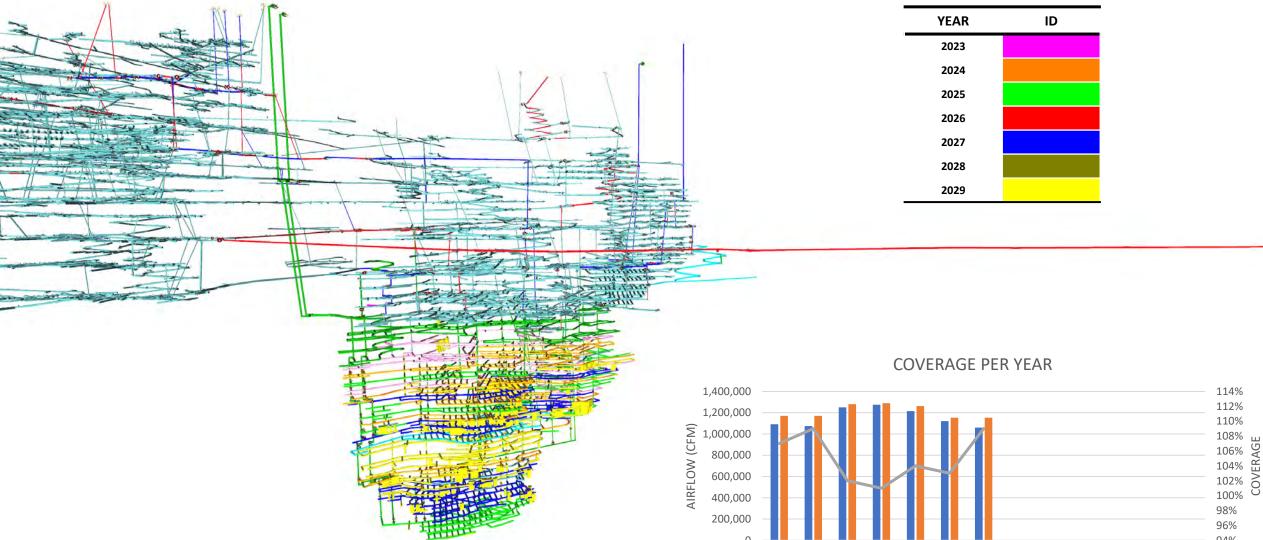




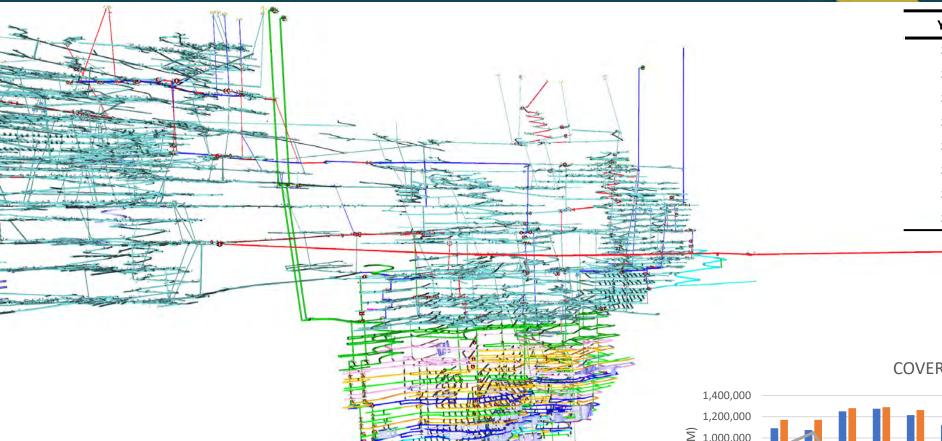
2023 2024 2025 2026 2027 2028 2029 2030 2031 2032 2033 2034 2035 YEAR

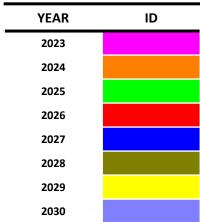
Coverage

Airflow Requirements CFM Airflow Intake

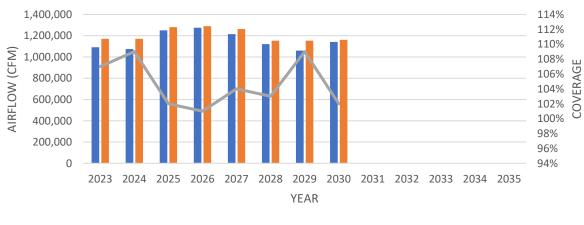






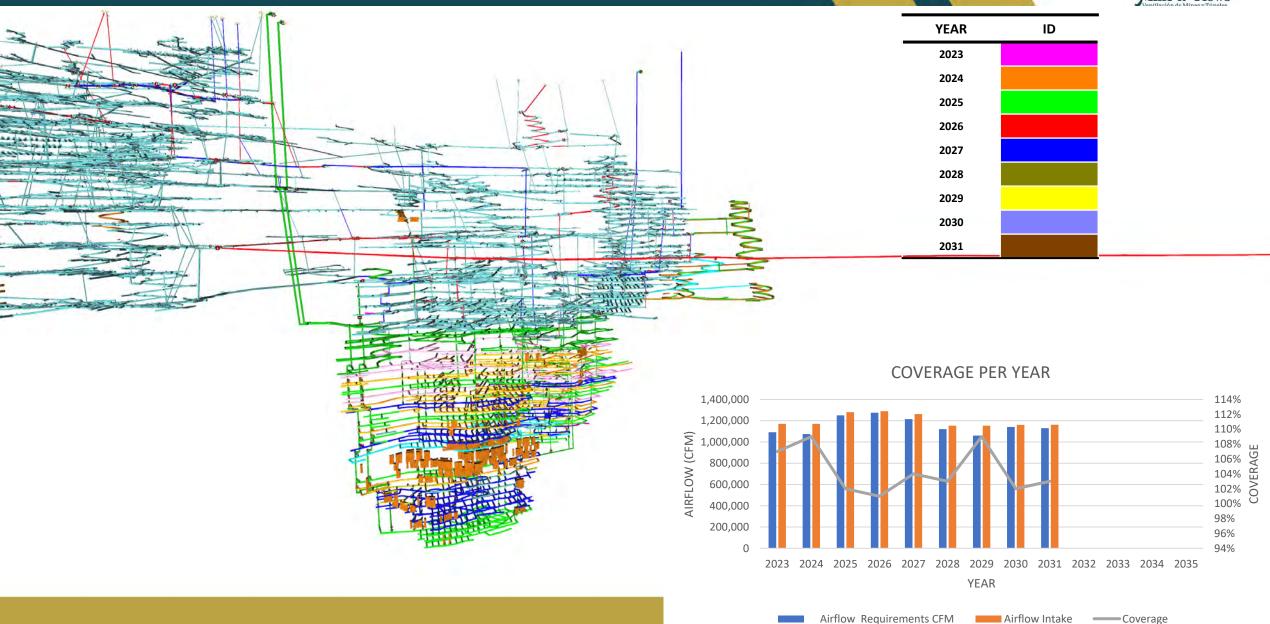


COVERAGE PER YEAR

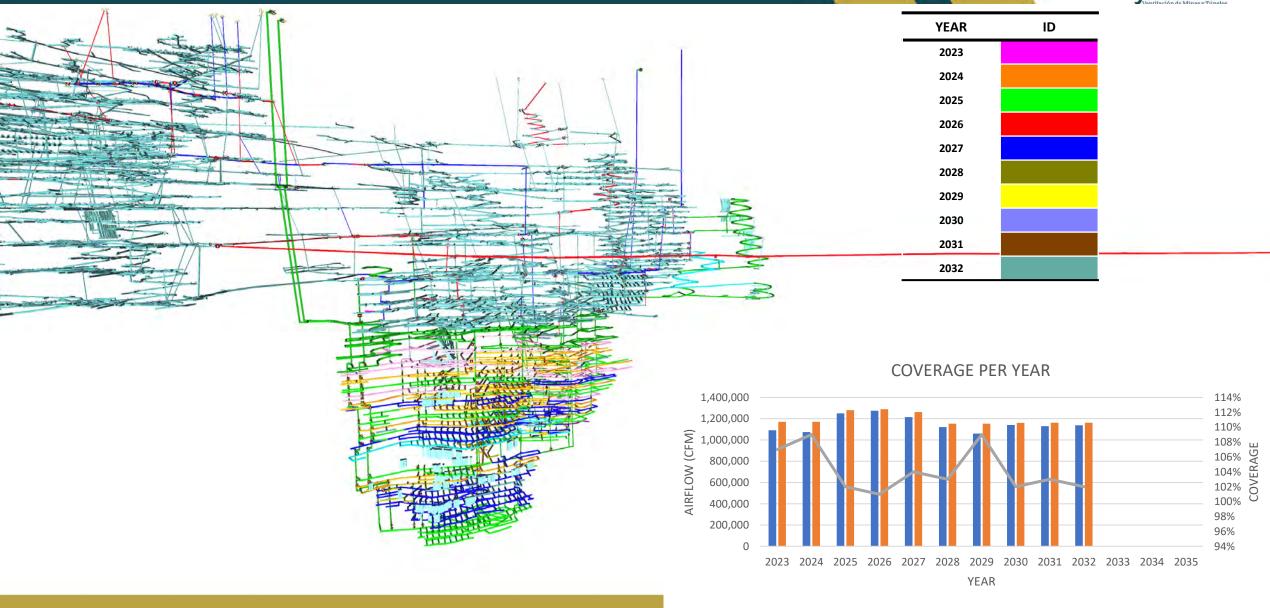


Airflow Requirements CFM Airflow Intake







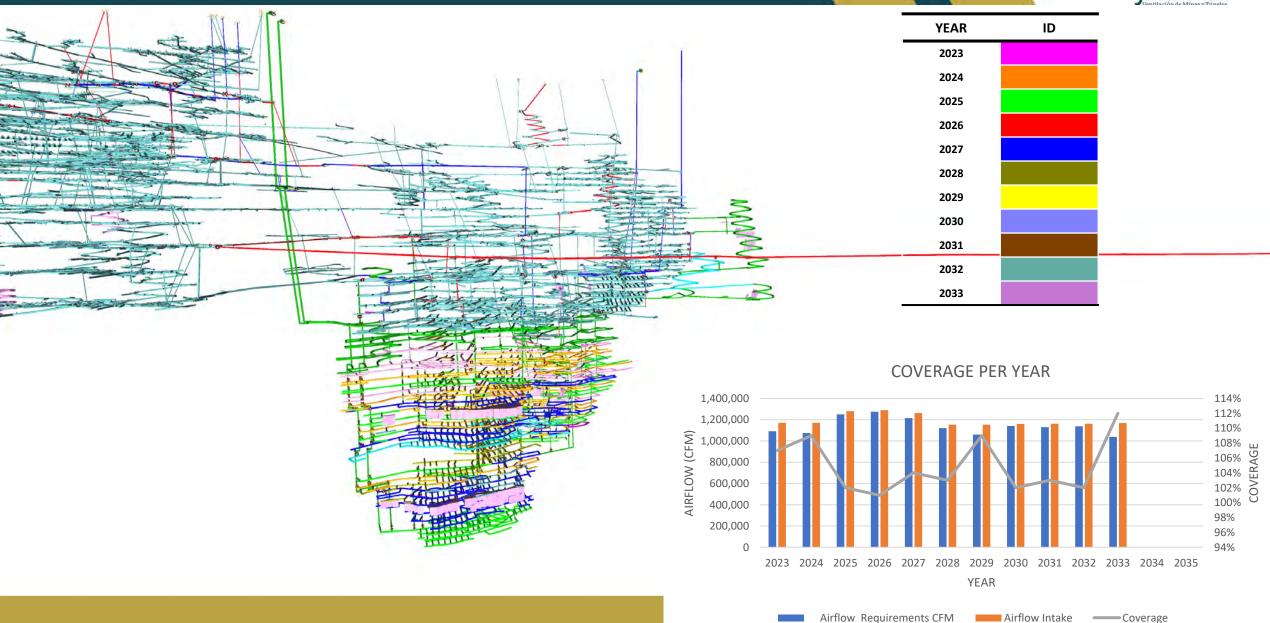


Airflow Requirements CFM

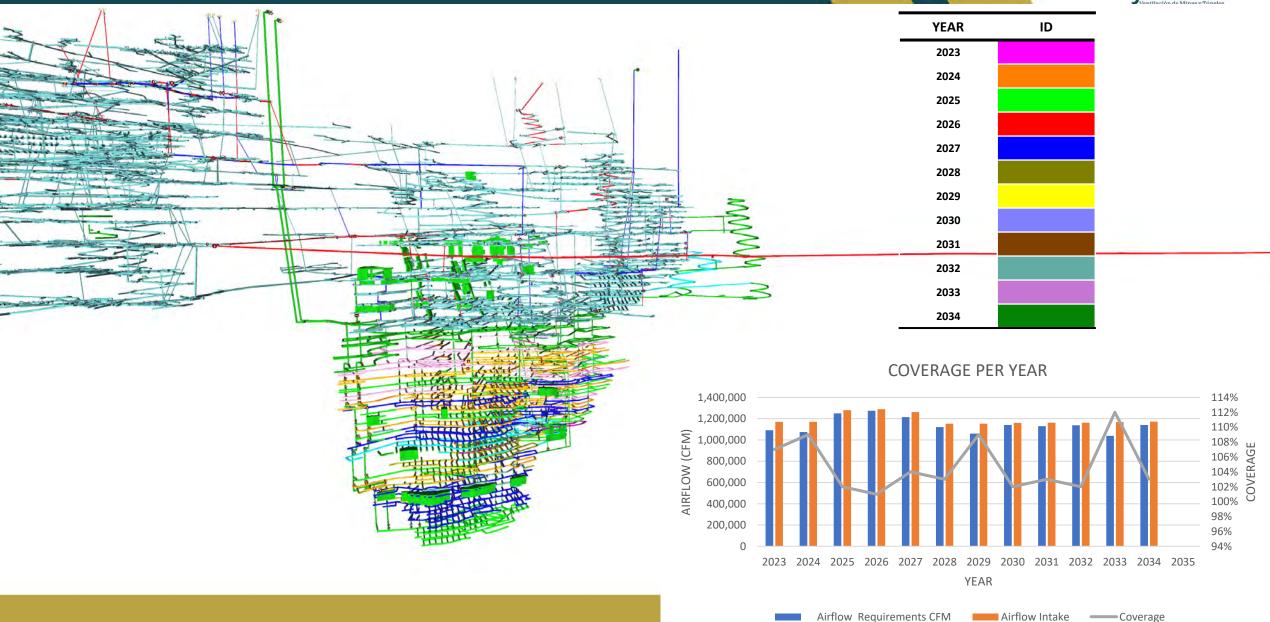
Airflow Intake



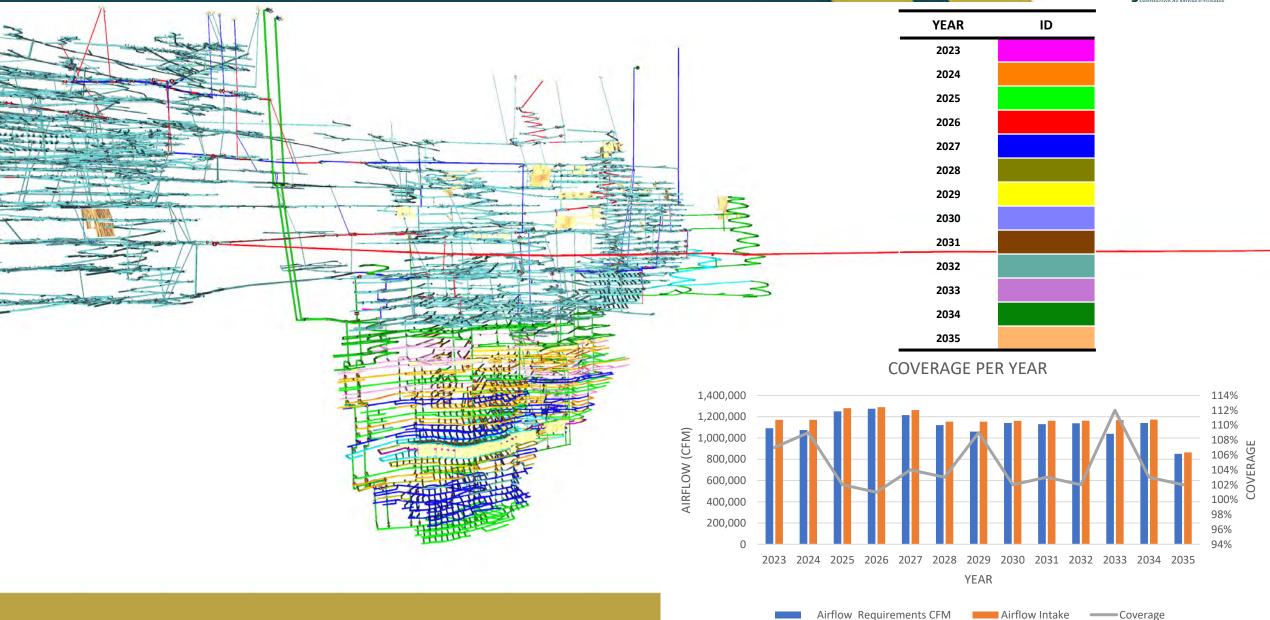
Airflow Intake











Conclusions



- The process of model construction and parameters calibration is fundamental to obtain a reliable model, adjusted to reality and accurate enough to be able to plan and simulate multiple scenarios, and find opportunities of improvement. Ventsim is a software that makes this process simple, practical and highly illustrative.
- After the assessment of multiple scenarios, the results converged in a trade-off analysis between the ventilation infrastructure (CAPEX) and the fan selection (power consumption OPEX), resulting in an important reduction of overall costs with respect to the initial estimations at the Prefeasibility Stage, with savings up to \$10.1 million in CAPEX and \$4.6 million in the net present value of the OPEX.
- Having the possibility to schedule the expansion of the mine ventilation system by years was a key
 part of the analysis in the estimation of the maximum airflow requirement over LOM, directly impacting
 in the decision of the economic diameter, and adjusting the fan operating point to what will be required,
 reducing a considerable amount of power consumption in benefit of the mine economics.

Future Work



The operator has been evaluating the need for a fire, heat and contaminants simulation process for the short-, mediumand long-term. However, given the uncertainty of certain operational parameters unrelated to the ventilation process, it may require some time before the decision is made and the next ventilation assessment takes place.



